

## Theoretical and Experimental Study of Reversible and Stable Wetting States of a Hierarchically Wrinkled Surface Tuned by Mechanical Strain

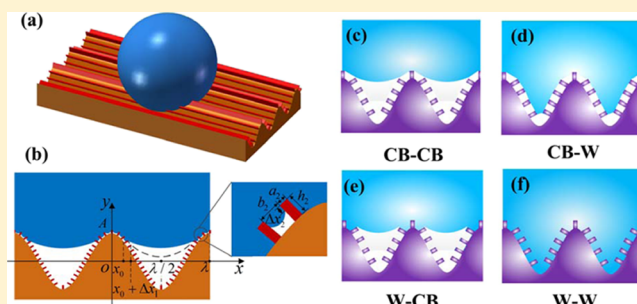
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### Supporting Information

**ABSTRACT:** The wetting behavior of hierarchically wrinkled surfaces has attracted great interest because of its broad application in flexible electronic, microfluidic chip, and biomedicine. However, theoretical studies concerning the relationship between the apparent contact angle and mechanical strain applied on the soft and flexible surface with a hierarchically wrinkled structure are still limited. We established a theoretical framework to describe and understand how prestrain and applied dynamic strain reversibly tune the wettability of the hierarchically wrinkled surface. More specifically, a direct relationship between the mechanical strain and contact angle was built through reversible tuning of the amplitude and the wavelength of the wrinkled structures caused by mechanical strain, which allowed for more precise adjustment of surface wettability. To verify the accuracy of the theoretical relationship between the contact angle and mechanical strain, a soft surface with a hierarchically wrinkled structure was prepared by combining wrinkled microstructures and strip ones. The results showed that the experimental contact angles were in agreement with the theoretical ones within a limited error range. This will be helpful for further investigation on the wettability of hierarchically wrinkled surfaces.



## INTRODUCTION

Wettability is one of the basic characteristics of a surface. The self-cleaning ability of the surface, removal of droplets, cell adhesion, and oil–water separation are all closely related to surface wettability.<sup>1–7</sup> Researchers find that the wettability of various surfaces is related to the surface energy and surface roughness, and the hierarchical structures with low surface energy and significant roughness make the surface superhydrophobic.<sup>8–11</sup> Research concerning the surface wettability of hierarchical structures of rigid materials is very thorough.<sup>12–18</sup> Compared with rigid materials, soft materials are more widely used in microfluidic chips,<sup>19–22</sup> soft robots,<sup>23</sup> wearable devices,<sup>24–27</sup> and so forth. However, studies concerning the surface wettability of soft materials have not been widely reported and further exploration is required.

Among the structures used to study the wettability of soft materials, wrinkled structures are the most common.<sup>28–31</sup> With regard to theoretical research concerning wrinkled surfaces, Liu et al. approximated a sine wave structure to study the relationship between the wrinkled size and surface wettability.<sup>32</sup> This theory was further extended to the analysis of the influence of different structures on wettability.<sup>33</sup> Zhang et al. employed the theories of structural wrinkling and solid–

liquid contact to design a hierarchically wrinkled surface which could be mechanically tuned between superhydrophilic and superhydrophobic by an applied strain.<sup>34</sup> However, they did not provide a wetting state diagram of hierarchically wrinkled surfaces nor did theoretically predict the relationship between the surface contact angle and applied strain to hierarchically wrinkled surfaces. In terms of experimental research, the hierarchical structures on the wrinkled soft surface are usually varied and prepared by using lithography, laser etching, chemical vapor deposition, and ultraviolet ozone treatment.<sup>35–39</sup> For example, Lin and Yang obtained hierarchical structures by depositing silicon nanoparticles on the wrinkled surface and found that the hierarchical structures not only improved the apparent contact angle but also decreased the contact angle hysteresis.<sup>40</sup> However, the uncontrollable size and morphology of the nanostructures and the use of expensive equipment limited the application of this method. Additionally, when utilizing the mechanical instabilities on the soft surface, some hierarchical structures can also be obtained.<sup>41–45</sup> For

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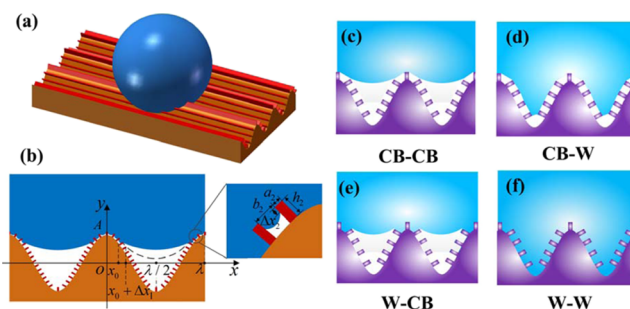
example, wrinkled structures with various sizes can be prepared from one template by the prestrain to generate well-defined and complex topological features.<sup>46,47</sup>

In practical applications, it is important to tune the wettability of the surface dynamically. A large number of studies show that the wettability of the surface can be controlled by external stimuli such as electric field, temperature, pH, ultraviolet light, and mechanical regulation.<sup>48–52</sup> Compared with temperature, pH, or light control, mechanical regulation is simpler and safer. There is also no special requirement for used materials and preparation processes. Zhao et al. fabricated hierarchically wrinkled surfaces on the polydimethylsiloxane (PDMS) film by photolithography and soft lithography. The increase in the mechanical strain with different directions resulted in the primary anisotropic wetting of the surface becoming isotropic or anisotropic dependent in the contact angle ranges from 120° to 138°.<sup>53</sup> Goel et al. prepared a silver-based wrinkled microstructure on the prestretched PDMS surface using the oblique deposition method, and the apparent contact angle could be reversibly changed from 126.2° to 154.8° (from hydrophobic to superhydrophobic) by adjusting the mechanical strain.<sup>54</sup> Unfortunately, the wetting state of the material surface was of instability during the multiple cycles. Therefore, the prediction of the wetting state of the surface of hierarchical structures and relationship between the contact angle and the strain via the theoretical investigation is necessary, which will be instructive and meaningful to the preparation of hierarchical structures with both a large range of contact angle variation and good repeatability under external strain.

In this study, a thermodynamic approach was used to analyze the wetting states of a droplet on the hierarchically wrinkled surface. We established a theoretical framework to understand how the prestrain and applied dynamic strain reversibly tune the wettability of the hierarchically wrinkled surface. We also experimentally prepared a hierarchically wrinkled surface through a prestretch process and template method with the wettability of the surface dynamically tuned from superhydrophobic to hydrophobic. After multiple stretching and release cycle tests, the experimental results were in agreement with the theoretical prediction. This will provide a theoretical guidance for reversible tuning of surface wettability in a controlled fashion used in microfluidic valves, micro- and nanofabrication of complex structures, and cell transport manipulation.

## THEORETICAL BASIS

**Wetting States of a Droplet on the Hierarchically Wrinkled Surface.** To analyze the wettability of the hierarchically wrinkled surface, as shown in Figure 1a, we establish a model of a droplet on surfaces with a wrinkled pattern and strip structures. We simplify the three-dimensional model to a two-dimensional one and just investigate the contact angle in the plane vertical to the strip direction. First, we analyze the cross section of the wrinkled structures with a droplet on it. Owing to the arc-shape of the top of wrinkled structures, the liquid level of the droplet will not form a tangent to the top of the wrinkled structures but will certainly wet some of the area (Figure 1b). Assume that the shape of the wrinkled structures matches a cosine function; then, the shape function of the solid surface can be expressed as  $y = A \cos\left(\frac{2\pi}{\lambda}x\right)$ . According to the previous studies,<sup>29,32,40,55</sup>



**Figure 1.** Schematic diagram of droplet infiltration and wetting states of a water droplet on a hierarchically wrinkled surface. (a) 3D schematic diagram of a droplet on the wrinkled surface with strip structures. (b) Schematic diagram of a general water droplet on a hierarchically wrinkled surface. (c–f) Wetting states of a water droplet on a hierarchically wrinkled surface: (c) CB–CB (Cassie–Baxter) state, (d) CB–W (Wenzel) state, (e) W–CB state, and (f) W–W state.

the wavelength  $\lambda$  and amplitude  $A$  can be written as  $\lambda = 2\pi h_f \left(\frac{\bar{E}_f}{3E_s}\right)^{1/3}$  and  $A = h_f \left(\frac{\epsilon}{\epsilon_c} - 1\right)^{1/2}$ . Here,  $h_f$  is the film thickness and  $\epsilon$  is the applied strain. The subscripts f and s refer to the top film (e.g., PDMS) and bottom substrate (e.g., viscous elastomer film VHB), respectively. In addition,  $\bar{E} = E/(1 - \nu^2)$  is the plane-strain modulus,  $E$  is the Young's modulus,  $\nu$  is the Poisson's ratio, and  $\epsilon_c = \frac{1}{4} \left(\frac{3E_s}{\bar{E}_f}\right)^{2/3}$  is the critical strain applied for the formation of wrinkles.<sup>56,57</sup>

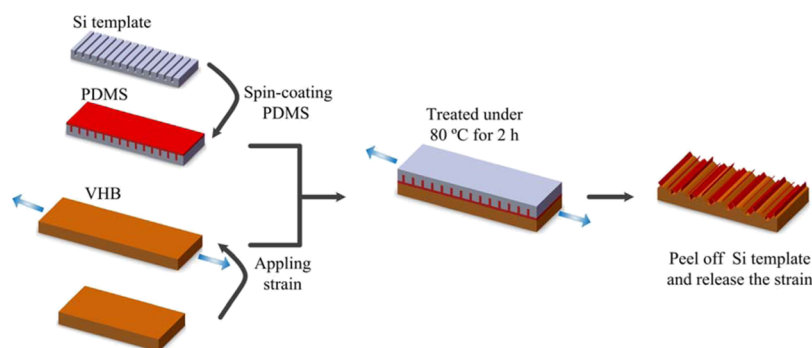
For a droplet on this surface,  $x_0$  ( $0 \leq \frac{x_0}{\lambda} \leq \frac{1}{2}$ ) is the liquid contact position, and  $\Delta x_1$  and  $\Delta x_2$  represent the infiltration depth of the droplet on the wrinkled structures and strip structures, respectively (Figure 1b).  $L_{\text{ext}}$  is the length of the outer surface of the droplet at the cross section. The geometrical relation can be obtained with  $L_{\text{ext}} = 2\theta R$ , where  $R$  is the radius of the droplet and  $\theta$  is the contact angle.  $L_{\text{base}}$  is the length of the contact between the droplet and substrate, and the geometrical relation is  $L_{\text{base}} = 2R \sin \theta$ .  $L_{\text{total}}$  corresponds to the total length of the substrate.<sup>15</sup> The schematic illustration of  $L_{\text{ext}}$ ,  $L_{\text{base}}$ , and  $L_{\text{total}}$  is shown in Figure S1. Assume that  $S$  is the area of the droplet cross section, and the relation between the radius  $R$  and the contact angle  $\theta$  is given by  $R = \sqrt{\frac{S}{\theta - \sin \theta \cos \theta}}$ .

Considering the strip structure of the hierarchically wrinkled surface, we denote the side length of the strip structure as  $a_2$ , with spacing  $b_2$  and strip height of  $h_2$ . Then, the total free energy of the system  $G$  includes the interfacial free energy and potential energy, which can be expressed as<sup>58</sup>

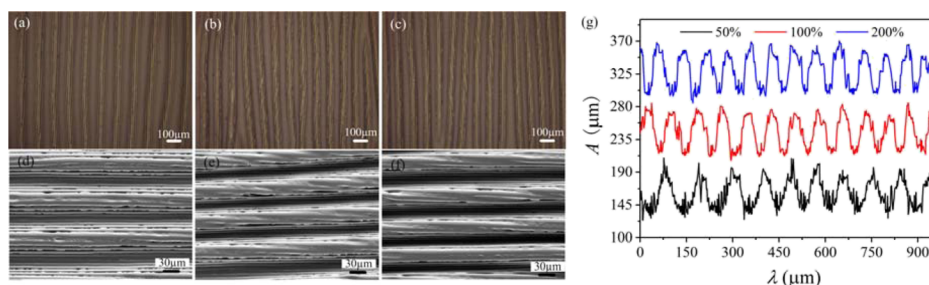
$$G = \gamma_{\text{LV}}L_{\text{LV}} + \gamma_{\text{SV}}L_{\text{SV}} + \gamma_{\text{SL}}L_{\text{SL}} \quad (1)$$

where  $\gamma_{\text{LV}}$ ,  $\gamma_{\text{SV}}$ , and  $\gamma_{\text{SL}}$  are the interfacial tension of the liquid–vapor interface, solid–vapor interface and solid–liquid interface, respectively.  $L_{\text{LV}}$ ,  $L_{\text{SV}}$ , and  $L_{\text{SL}}$  are the length of the liquid–vapor interface, solid–vapor interface, and solid–liquid interface, respectively.

**Equation of Contact Angle.** For a droplet on a rough surface, it is either in a Wenzel (W) state or in a CB state.<sup>59,60</sup> Taking into account the different positions of the triple contact point  $x_0$ ,  $\Delta x_1$ , and  $\Delta x_2$  in this model, the droplets will be in different wetting states. In our previous study,<sup>10,11</sup> a



**Figure 2.** Schematic description of preparation of hierarchically wrinkled surface by the relaxation of PDMS film with strip structures on the prestretched VHB film.



**Figure 3.** Characterization of the hierarchically wrinkled surfaces with different amounts of prestrain. (a–c) Laser microscopy images of the hierarchically wrinkled surfaces with different amounts of prestrain: (a)  $\epsilon_{\text{pre}} = 50\%$ , (b)  $\epsilon_{\text{pre}} = 100\%$ , (c)  $\epsilon_{\text{pre}} = 200\%$ . (d–f) High magnified SEM images of the hierarchically wrinkled surfaces with different amounts of prestrain: (d)  $\epsilon_{\text{pre}} = 50\%$ , (e)  $\epsilon_{\text{pre}} = 100\%$ , (f)  $\epsilon_{\text{pre}} = 200\%$ . The width and height of strip structures are 10 and 10  $\mu\text{m}$ , respectively. (g) Numerical results from laser microscope of hierarchically wrinkled surfaces with different amounts of prestrain. The black, red, and blue lines represent the amount of prestrain of 50, 100, and 200%, respectively. The relative wrinkled height of the samples is  $A/\lambda = 0.247$ ,  $A/\lambda = 0.355$ , and  $A/\lambda = 0.435$ , respectively.

thermodynamic approach was used to analyze all wetting states of a water droplet on dual-scale rough surfaces with structured sidewalls. This method is also suitable here. Detailed derivation is described in Part S1 of the [Supporting Information](#).

According to the principle of minimum free energy<sup>61</sup> and [eq 1](#), the wetting states include four stable states, namely, CB–CB, CB–W, W–CB, and W–W states, as shown in [Figure 1c–f](#). The front symbol represents the wetting state of strip structure, and the back one represents the wetting state of wrinkled structure. The contact angle equation of the four wetting states can be expressed as follows

$$\cos \theta_{\text{CB–CB}} = r_f f_1 f_2 \cos \theta_0 + r_f f_1 f_2 - r_f f_1 + f_1 - 1 \quad (2)$$

$$\cos \theta_{\text{CB–W}} = r_f f_2 \cos \theta_0 + r_f f_2 - r_1 \quad (3)$$

$$\cos \theta_{\text{W–CB}} = r_f r_2 f_1 \cos \theta_0 + f_1 - 1 \quad (4)$$

$$\cos \theta_{\text{W–W}} = r_1 r_2 \cos \theta_0 \quad (5)$$

Here,  $f$  is the length fraction that can be given by  $f_1 = \frac{2x_0}{\lambda}$ ,  $f_2 = \frac{a_2}{a_2 + b_2}$ ,  $r$  is the rough factor that is given by  $r_1 = \frac{\int_{-\lambda/2}^{\lambda/2} \sqrt{1 + y'^2} dx}{\lambda}$ ,  $r_2 = \frac{a_2 + b_2 + 2h_2}{a_2 + b_2}$ ,  $r_f = \frac{\int_{-x_0}^{x_0} \sqrt{1 + y'^2} dx}{2x_0}$ .  $\theta_0$  is the intrinsic contact angle and  $y'$  is the derivative of  $y$  ( $y = A \cos(\frac{2\pi}{\lambda}x)$ ). Furthermore, because of the flexibility of the substrate, the prestretch  $\epsilon$  can affect the relative height ( $A/\lambda$ ) so that the  $\theta$  is also altered. Because of these unique features, precise control of the  $\theta$  with the wrinkled surface becomes possible.<sup>62</sup>

$$\frac{A}{\lambda} = \frac{1}{\pi} \sqrt{\epsilon - \epsilon_c} \quad (6)$$

By substituting [eq 6](#) into the  $\theta$  in different wetting states, the relationship between the prestrain  $\epsilon$  and  $\theta$  can be obtained.

## EXPERIMENTAL SECTION

**Preparation of the PDMS Solution.** The PDMS solution was prepared by mixing a prepolymer (Sylgard 184, Dow Corning) with a curing agent in a 10:1 ratio at room temperature and degassed in a vacuum oven for 30 min to remove all bubbles from the viscous liquid.

**Preparation of Hierarchically Wrinkled Substrates.** The fabrication process for the hierarchically wrinkled surface is shown in [Figure 2](#). The commercial Si templates with strip structures were fabricated by the wet etching technique. The width and height of strip structures were 10 and 10  $\mu\text{m}$ , respectively, and the strip spacing was 3, 5, 10, and 20  $\mu\text{m}$ , respectively. After immersion in “piranha” etch solution (70%  $\text{H}_2\text{SO}_4$ , 30%  $\text{H}_2\text{O}_2$ , 90  $^\circ\text{C}$ ), the patterned Si template was cleaned with deionized water and then immersed into a solution consisting of 10 mL of *n*-heptane, 0.2 mL of trimethoxyoctadecylsilane, and 0.5 mL of ethyl acetate for 2 h for hydrophobic treatment. Then, the Si template was annealed in an oven at 100  $^\circ\text{C}$  for 1 h. The well-prepared PDMS solution was spin-coated on the Si template at 8000 rpm for 20 s. The thickness of the PDMS film was controlled about 150  $\mu\text{m}$ . Next, the Si template with covered PDMS was placed into the oven and cured for 8 min at 80  $^\circ\text{C}$ . After the PDMS side was adhered onto a prestretched viscous elastomer film (VHB 4910, 3 M Inc., US) by a clamp device ([Figure S2a](#)), the amount of prestrain was easy controlled by the clamp device, they were put into the oven together and cured for 2 h at 80  $^\circ\text{C}$ . During this process, the strain was kept by the clamp device. After cooling and peeling off the Si template, the patterned PDMS film was transferred onto the prestretched VHB film. Finally, the strain was slowly released and

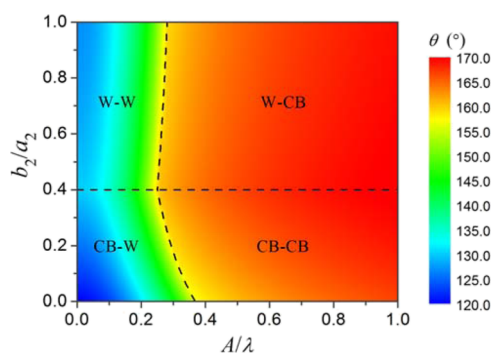


the wrinkled structures with the strip structures were formed from the internal buckling of the PDMS elastomer film. The wrinkled PDMS films without the strip structures were also prepared for control experiments.

**Characterization.** The morphologies of the hierarchically wrinkled surfaces with different amounts of prestrain were analyzed by a laser microscope (Keyence, VK-X100, Figure 3a–c) and scanning electron microscopy (SEM, Hitachi S4800, Figure 3d–f). The droplet contact angle ( $\theta$ ) was measured using 4  $\mu$ L of droplets of deionized water with a contact angle instrument (Thermo, DCA-322). The water drops were dispensed using a syringe pump through a needle with 100  $\mu$ m inner diameter. It can be seen from Figure 3a–f that as the amount of prestrain increases, the wavelength ( $\lambda$ ) of the structure decreases. Numerical results from a laser microscope (Figure 3g) show that the relative height ( $A/\lambda$ ) of the wrinkled structures gradually increases with increasing amount of prestretching. Comparing the numerical results of the wrinkled structures with and without the strip structures under the same amount of prestrain (Figure S3-1), it can be seen that the strip structure has a little effect on the size of the wrinkled structure. The morphologies of the strip structures and their respective  $\theta$  are shown in Figure S3-2a–d. The morphologies of the hierarchically wrinkled surfaces and their respective  $\theta$  are shown in Figure S3-2e–h. We find that as the spacing increases, the change in  $\theta$  shows a tendency to increase first and then decrease.

## RESULTS AND DISCUSSION

Lotus leaves have excellent superhydrophobicity, largely because of the droplets on the surface being in a CB state with a big contact angle.<sup>8,9</sup> Therefore, it is of great importance to the stability of superhydrophobic surfaces that the droplet remains in a CB–CB state as much as possible. This should be possible by controlling the size of the wrinkle and strip structures. To further analyze the influence of the size of the structures on the wetting states of the droplets, we assign  $0 \leq b_2/a_2 \leq 1$ ,  $0 \leq A/\lambda \leq 1$  and an intrinsic contact angle  $\theta_0 = 120^\circ$ . Figure 4 shows the wetting phase diagram of four stable



**Figure 4.** Wetting phase diagram of four stable wetting states. The apparent contact angle ( $\theta$ ) of a water droplet on the surface in four stable wetting states, as a function of the relative spacing of wrinkled strip structures.

wetting states of the droplet which can be divided into four regions. When  $A/\lambda \leq 0.3$ , the  $\theta$  is much lower than that in the case of  $0.3 \leq A/\lambda \leq 1$ . In the following section, the relationship between the size of each structure and  $\theta$  will be discussed.

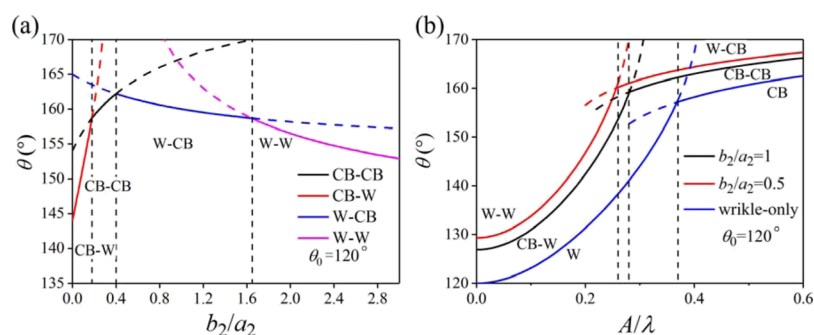
As shown in Figure 5a, taking  $A/\lambda = 0.3$ , changing the spacing between strips ( $b_2$ ) at a fixed width ( $a_2$ ), and when  $0 \leq b_2/a_2 \leq 0.18$ , the droplets are in a CB–W state. From a thermodynamic point of view, the droplets tend to wet the wrinkled structures. The droplets then attain a CB–CB state when  $0.18 \leq b_2/a_2 \leq 0.4$ , and the  $\theta$  reaches a peak ( $163^\circ$ ) with

the increase of  $b_2/a_2$ . However, as the spacing of the strip structures continues to increase ( $0.4 \leq b_2/a_2 \leq 1.65$ ),  $\theta$  begins to decrease from  $164^\circ$  to  $159^\circ$ . At this point, the droplets exist in a W–CB state. Similarly,  $\theta$  still decreases with the increasing spacing of the strip structures when the droplets exist in a W–W state. In addition, the wetting state of the strip surface changes from CB to W following an increase in the size of the strip. The wetting state of the wrinkled structure changes from W to CB first and then from CB to W. This shows that the change in the size of the strip structures will affect the wetting states of the wrinkled structures, and as the  $b_2/a_2$  increases, the contact angle increases first and then decreases. Besides, the effect of the strip height on wetting states is shown in Figure S4. It can be seen that as the  $h_2/a_2$  increases, the range of  $b_2/a_2$  in which the droplets are in the CB–CB state becomes larger.

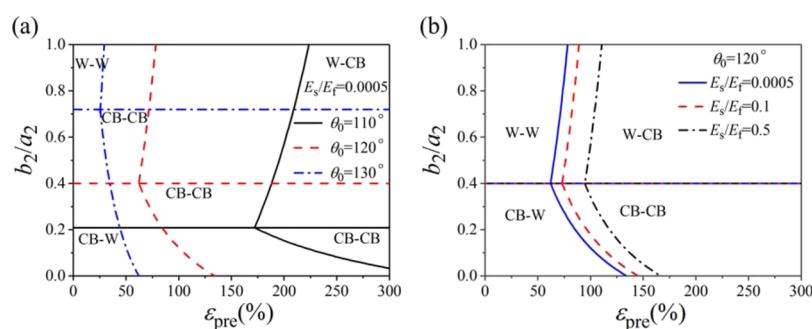
Likewise, if the size of the strip remains unchanged, the change in the size of the wrinkled structures will also affect the wetting state of the droplets, as shown in Figure 5b. Following a change in the strip's size, the analysis result from a thermodynamic point of view shows that the wetting states of the droplets can be divided into two regions. When  $b_2/a_2 = 0.5$  and  $A/\lambda = 0.26$ , the droplets are in a W–W state, indicating that the strip and wrinkled structure are both wetted. When  $A/\lambda \geq 0.26$ , the droplets are in a W–CB state, indicating that the strip structures are being wetted but the wrinkled structures are not being immersed. Following a change in the size of the strip structure, it is possible to find “point-of-variability”. At the left of the point,  $\theta$  of the droplet increases sharply and the wrinkled structure is in a Wenzel state. Conversely, it can be found that the wetting state of the strip structures does not change with a change in the size of the wrinkled structures. The transition of the wetting state involves the change of the energy barrier. The detailed analysis of the energy barrier is shown in Part S5 in the Supporting Information. Our results indicate that the wrinkled structure and strip structures increase the stability of the structure. On the other hand, under the same deformation, different sized strip structures show different contact angle ranges. Therefore, strip structures of an appropriate size are conducive to broadening the tunable range of the  $\theta$ .

### Influence of the Intrinsic Contact Angle and Elastic Modulus on the Wetting States.

As discussed above, the sizes of the strip structures and wrinkled structures affect the wettability of the surface. The structure of the strips can be controlled by soft lithography. However, the relationship between the size of the wrinkled structure and prestretch must be determined. We chose the VHB and PDMS system for investigation. According to the different Young's modulus between a film and a substrate, compared with theory<sup>63</sup> (Figure S6), the size of the wrinkled structures can be found to be in good agreement with the theoretical values and within the allowed range of error. Following an increase in the ratio of the elastic modulus  $E_s/E_p$ , a wrinkled pattern is more difficult to form, but the size of the wrinkled structure  $A/\lambda$  increases as a result of the increasing prestretch. Moreover, the ratio of the elastic modulus  $E_s/E_f$  of the selected materials (VHB and PDMS) is approximately  $5 \times 10^{-4}$ , and further increasing this ratio does not alter the theoretical prediction. Besides, because of the high adhesion of VHB and flexibility of PDMS, there is no delamination between materials under strain during the experiment. These suggest that the two materials, VHB and PDMS, are suitable for the fabrication of wrinkled structures.



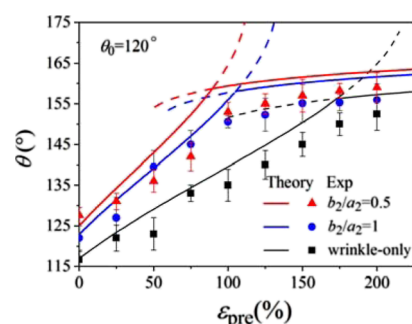
**Figure 5.** (a) Relationship between the size of strip  $b_2/a_2$  and apparent contact angle  $\theta$  with  $A/\lambda = 0.3$ . (b) Relationship between the apparent contact angle  $\theta$  and the size of the wrinkled structure  $A/\lambda$  at different strip structures ( $b_2/a_2$ ).



**Figure 6.** Phase diagram depicting the influence of (a) intrinsic contact angle  $\theta_0$  and (b) elastic modulus of the substrate on the wetting state. The amount of prestrain  $\epsilon_{pre}$  can be converted to  $A/\lambda$  using Figure S6.

Not only does the elastic modulus of the substrate affect the wettability of the hierarchically wrinkled surface but also the intrinsic contact angle  $\theta_0$  also influences it. Figure 6 shows the impact of the  $\theta_0$  and the ratio of the elastic modulus of the substrates on the CB–CB state. Following an increase in the  $\theta_0$  (Figure 6a), the region corresponding to the CB–CB state also increases, indicating that it is beneficial to maintaining a CB–CB state of the droplet on the surface. The CB–CB area gradually increases following a decrease in the ratio of the elastic modulus  $E_s/E_f$  (Figure 6b), indicating that the film becomes harder or the substrate becomes softer; these phenomena are both conducive to maintaining a CB–CB state. The prestretch  $\epsilon_{pre}$  in Figure 6 can be converted to  $A/\lambda$  using Figure S6. Superhydrophobic surfaces can therefore be reasonably designed via the selection of the intrinsic contact angle and elastic modulus of the substrate.

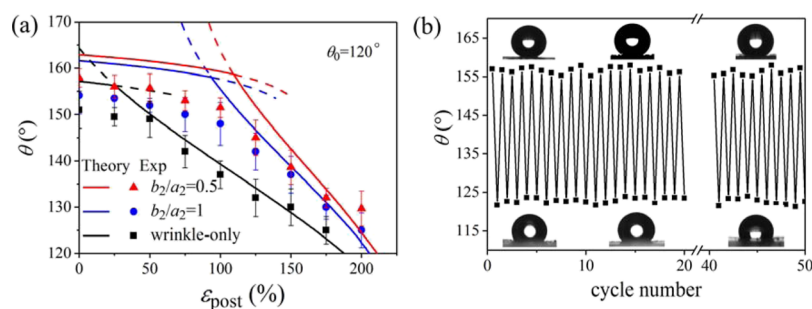
**Influence of Prestretch on the Wettability of the Hierarchically Wrinkled Surface.** The wetting of a water drop on the hierarchically wrinkled surface was investigated at different amounts of prestrain and dynamic strain. Pictures of stretching and unloading in a real system are shown in Figure S2b–d. Figure 7 shows the experimentally observed and theoretically determined  $\theta$  of the hierarchically wrinkled surface for different amounts of prestrain when  $\theta_0 = 120^\circ$ . Control experiments were conducted on the wrinkled surfaces without a strip structure. During a gradual increase in prestretching, the wetting state of the droplet on the hierarchically wrinkled surface changes from the W–W state to W–CB one, and the  $\theta$  changes from  $126^\circ$  to nearly  $165^\circ$  in terms of theory. The increase in hydrophobicity is caused by the enhancement of the relative height of the wrinkled structure; the strip structures are wetted while the wrinkled structures are in the CB state following prestretching. Within the limit of allowable errors, our contact angle equations



**Figure 7.** Relationship between the apparent contact angle  $\theta$  and the amount of prestrain  $\epsilon_{pre}$ . In terms of theory,  $\theta$  increases from  $124^\circ$  to  $165^\circ$  with the increasing amount of prestrain. The spot on the graph is the experimental value, with the intrinsic contact angle  $\theta_0 = 120^\circ$  of the substrate.

shown in eqs 2–5 are in good agreement with experimentally observed values. This demonstrates that the superhydrophobicity can be achieved using a hierarchically wrinkled surface and that the  $\theta$  is tunable by controlling the prestretch.

**Influence of Applied Stretching on the Wettability of the Hierarchically Wrinkled Surface.** Another advantage of this hierarchically wrinkled surface is that dynamic strain can be applied so that the  $\theta$  can be adjusted accordingly. At the amount of prestretch of 200%, stable repulsive superhydrophobicity is achieved, resulting in a static contact angle in excess of  $150^\circ$  (Figure 8a). As the amount of dynamic strain increases, the  $\theta$  decreases in line with a decrease in the relative height of the wrinkled structures. When the amount of dynamic strain is lower than a threshold value, the droplets on the hierarchically wrinkled surface are in a W–CB state. As the dynamic strain is applied, the droplets preferentially wet the



**Figure 8.** (a) Relationship between the apparent contact angle  $\theta$  and amount of dynamic strain  $\epsilon_{\text{post}}$ . The spot on the graph is the experimental value, with the intrinsic contact angle of the substrate  $\theta_0 = 120^\circ$ .  $\theta$  decreases from  $157^\circ$  to  $124^\circ$  as  $\epsilon_{\text{post}}$  increases. (b) Fully reversible cyclic switching of  $\theta$  by applying a dynamic strain of 200% and relaxation. The substrate was prestretched at 200%, and the  $\theta$  changes from approximately  $157^\circ$  to  $123^\circ$ .

wrinkled pattern so that the wetting states change from W–CB to W–W.

Because of the excellent elastic recovery of the VHB substrate, multiple stretching and releasing cycles were applied. Cyclic dynamic switching was conducted at 200% prestretching of the substrate by periodic application of 200% dynamic strain and relaxation. First, the soft substrate was gradually stretched to three times as long as its original length, and then, the dynamic strain was released.  $\theta$  is consistently tuned from  $157^\circ$  to  $123^\circ$  between each cycle, namely, from superhydrophobic to hydrophobic. As can be seen from Figure 8b, even if the stretching–releasing cycle was applied repeatedly over 50 cycles, the surface retains the wettability. This suggests that the wetting switch is reversible and that the hierarchically wrinkled surface is tunable and stable.

## CONCLUSIONS

In conclusion, a theoretical framework was established to understand how the prestrain and applied dynamic strain reversibly tunes the wettability of a hierarchically wrinkled surface. Specifically, we first established the relationship between the contact angle and structural size using a thermodynamic equation, which included the wrinkling structure size and strip structure size; we then established the relationship between strain and wrinkled structure size and the relationship between strain and contact angle. Through theoretical analysis and related experiments, we have shown that the wettability of the surface can be controlled by applying different amounts of prestretch and external strain, which can mostly be attributed to the change in structural the size and energy barrier. Furthermore, the surface wettability can be adjusted from superhydrophobic to hydrophobic, even after multiple stretching–release cycles. This research may provide insights into the design of soft surfaces for tunable wetting and motivate further research for mechanically tunable surfaces.

## ASSOCIATED CONTENT

### Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acs.langmuir.9b00599.

Thermodynamic analysis of wetting states on the hierarchically wrinkled surface, experimental setup, laser micrograph of the wrinkled structures and hierarchically wrinkled structures under the same amount of prestrain, morphology of the strip structures and the hierarchically wrinkled surfaces and their

respective apparent contact angle, effect of strip height on wetting states, analysis of the energy barrier in the wetting transition, and relationship between prestretching and the size of the wrinkled structure (PDF)

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### Notes

The authors declare no competing financial interest.

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